

ERYING-POWELL FLUID SLIP FLOW WITH TEMPERATURE AND SPACE DEPENDENT HEAT GENERATION

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Abstract: An analysis was made to study the effects of slip fluid flow and time dependent heat generation/absorption parameter on an incompressible Eyring-Powell fluid. The boundary layer equations governed by the incompressible fluid flow is converted to dimensionless employing similarity transformations. The ultimate equations are solved using bvp4c method. The upshots of this analysis for various dimensionless material parameters on the flow field were elaborately discussed with the help of graphs and tables.

Keywords: Eyring-Powell fluid, Non-Newtonian, Slip flow, heat generation/absorption, boundary value problem

Introduction: Non-Newtonian fluids have great importance because of its diversity in nature in terms of their viscous and elastic properties. A great attention was given by the researchers now-a-days on one of the non-Newtonian fluid called “Eyring-Powell fluid”. This fluid model distinct itself from other non-Newtonian fluid models because it is a consequent from kinetic theory of liquids in spite of empirical relation. In addition, this fluid can be reduced to Newtonian behaviour for low and high shear rates. The Cauchy stress tensor, in as Eyring-Powell fluid [1] takes the following form:

$$\lambda_{ij} = \mu \frac{\partial u_i}{\partial x_j} + \frac{1}{\beta} \sinh^{-1} \left(\frac{1}{C} \frac{\partial u_i}{\partial x_j} \right) \quad (1)$$

where μ is dynamic viscosity and β and C are the rheological fluid parameters of the Eyring-Powell fluid model.

Consider the second-order approximation of the \sinh function as follows:

$$\sinh^{-1} \left(\frac{1}{C} \frac{\partial u_i}{\partial x_j} \right) \cong \frac{1}{C} \frac{\partial u_i}{\partial x_j} - \frac{1}{6} \left(\frac{1}{C} \frac{\partial u_i}{\partial x_j} \right)^3, \left| \frac{1}{C} \frac{\partial u_i}{\partial x_j} \right| \ll 1 \quad (2)$$

The introduction of the appropriate terms into the flow model is considered next. The resulting boundary value problem is found to be well-posed and permits an excellent mechanism for the assessment of rheological characteristics on the flow behaviour. A rich research text on Eyring -Powell fluid on different geometries and applications are available in literature [2]-[4]. Vittal et al. [5] analyzed the stagnation point flow of a MHD Powell-Eyring fluid over a nonlinearly stretching sheet in the presence of heat source/sink. Mahanthesh et al. [6] studied the effect of a nanoEyring-Powell fluid past a convectively heated stretching sheet in the presence of thermal radiation, viscous dissipation and Joule heating. El-Aziz et al. [7] investigated heat transfer effects with space- or-temperature-dependent heat source in a mixed convection flow. The space and temperature-dependent heat generation/absorption (non-uniform heat source/sink) q''' is defined as

$$q''' = \left(\frac{kU_w(x)}{xv} \right) (A^*(T_w - T_\infty) f' + B^*(T - T_\infty)) \quad (3)$$

where A^* and B^* are parameters of the space and temperature dependent internal heat generation/absorption. The positive and negative values of A^* and B^* represents generation and absorption, respectively. Tsai et al. [8] investigated the flow and heat transfer over an unsteady stretching surface with non-uniform heat source. Khader and Megahed [9] studied the heat transfer of the Powell-Eyring fluid thin film over an unsteady stretching sheet with internal heat generation using the Chebyshev finite difference method. El-Aziz and Salem [7] studied the MHD-mixed convection and mass transfer from a vertical stretching sheet with diffusion of chemically reactive species and space- or temperature-dependent heat source. Abel et al. [10] analysed the heat transfer in MHD viscoelastic boundary layer flow over a stretching sheet with non-uniform heat source/sink.

On the other hand, in certain circumstances, the partial slip between the fluid and the moving surface may occur in situations when the fluid is particulate such as emulsions, suspensions, foam and polymer solutions. In these cases, the proper boundary condition is replaced by Navier’s condition, where the amount of relative slip is proportional to local shear stress. Bhaskar Reddy et al. [11] analysed the influence of Variable thermal conductivity on MHD boundary layer Slip flow of Ethylene-Glycol based Cu nanofluids past a stretching sheet with convective boundary condition. Sreenivasulu et al. [12] studied the influence of Magnetic Field on a Nanofluid Past a non Linear Stretching Sheet with Uniform Heat Source. The earlier studies that took into account the slip boundary condition over a stretching sheet were conducted by Andersson [13]. He gave a closed form solution of a full Navier-Stokes equations for a magnetohydrodynamics flow over a stretching sheet. Following Andersson, Wang [14] found the closed form similarity solution of a full Navier-Stoke’s equations for the flow due to a stretching sheet with partial slip.

In view of the above observations, an attempt is made to study the effects of Navier’s slip on Eyring-Powell fluid past a stretching surface with temperature-space dependent heat generation.

2. Mathematical Formulation: An incompressible and electrically conducting two dimensional boundary layer flow of an Eyring-Powell fluid past a stretching sheet with partial slip and temperature dependent non-uniform heat generation/absorption is considered. An external magnetic field $B(x)$ is applied along the y direction. A non-uniform heat source/sink q''' is taken into account which depends upon space and temperature. There is a constant suction/injection velocity V_w normal to the sheet. The boundary layer equations that govern the present flow subject to the Boussinesq’s approximations can be expressed as

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0 \tag{4}$$

$$u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} = \left(\nu + \frac{1}{\rho \beta C^*} \right) \frac{\partial^2 u}{\partial y^2} - \frac{1}{2\rho \beta C^{*3}} \left(\frac{\partial u}{\partial y} \right)^2 \frac{\partial^2 u}{\partial y^2} - \frac{\sigma B_0^2}{\rho} u \tag{5}$$

$$u \frac{\partial T}{\partial x} + v \frac{\partial T}{\partial y} = \alpha \frac{\partial^2 T}{\partial y^2} + q''' \tag{6}$$

The corresponding boundary conditions are

$$u = u_w + Nv_f \frac{\partial u}{\partial y}; \quad v = -V_w; \quad T = T_w(x) = T_\infty + bx \quad \text{at } y=0 \tag{7}$$

$$u = 0; \quad T \rightarrow T_\infty \quad \text{as } y \rightarrow \infty$$

where u, v are the velocity components in the x and y directions, respectively, T - the temperature of the nanofluid, T_∞ - the ambient fluid temperature, σ - the electric conductivity, B_0 - the uniform magnetic field strength

Introducing the similarity transformations,

$$\eta = \sqrt{\frac{c}{\nu}} y, \quad u = cxf'(\eta), \quad v = -\sqrt{cv}f(\eta), \quad \theta(\eta) = \frac{T - T_\infty}{T_w - T_\infty} \tag{8}$$

$$M = \frac{\sigma B_0^2}{c\rho}, \quad \Gamma = \frac{x^2 c^3}{2\nu C^{*2}}, \quad K = \frac{1}{\mu \beta C^*}, \quad V_w = \frac{v_0}{\sqrt{bc}}, \quad \text{Re} = \frac{xU_w(x,t)}{\nu}$$

Equations (3)-(6) become

$$(1 + K)f''' + ff'' - f'^2 - K\Gamma f''f''' - Mff' = 0 \tag{9}$$

$$\theta'' - \text{Pr}(f'\theta - f\theta') + A^*f' + B^*\theta = 0 \tag{10}$$

The associated boundary conditions

$$f' = 1 + \delta f''; \quad f = S; \quad \theta = 1 \quad \text{at } \eta = 0 \tag{11}$$

$$f' \rightarrow 0, \theta \rightarrow 0 \quad \text{as } \eta \rightarrow \infty$$

Equation (8) is subject to the constraint $\Gamma K \ll 1$ according to Javed et al. [3].

The quantities of practical interest in this study are the skin friction or the shear stress coefficient C_f and the local Nusselt number Nu , which are defined in dimensionless form as

$$\sqrt{\text{Re}} C_f = - \left[(1 + K)f''(0) - \frac{K\Gamma}{3} f'''(0) \right], \quad \frac{Nu}{\sqrt{\text{Re}}} = -\theta'(0) \tag{12}$$

RESULTS AND DISCUSSIONS

The governing boundary layer equations (9) and (10) subject to the boundary conditions (11) is solved numerically by employing bvp4c method. In order to get a physical insight into the problem, a

representative set of numerical results are computed and depicted graphically in Figs.1-6. In order to test the accuracy of our results, we compared it with the existed literature (Mahapatra and Gupta [15] and Raju et al.[16]), it is observed that the present results show an excellent correlation agreement with previous study (Table 1).

Figs. 1 -2 describe the effect of fluid parameter K on the velocity and temperature profiles. From Fig. 4, it can be seen that the velocity field and boundary layer thickness are increasing functions of K , whereas the temperature boundary thickness reduce thereby decreasing the fluid temperature (Fig.2). Figs. 3 and 4 illustrate the variation of the stream wise velocity and temperature for different values of velocity slip parameter λ . As slip parameter increases, the velocity of the flow at the surface decreases because under the slip condition, the pulling of the stretching sheet can be only partly transmitted to the fluid and converges swiftly (Fig.3). Physically, when slip occurs, the flow velocity near the sheet is no longer equal to the stretching velocity of the sheet and the differences between the wall and the fluid velocities near to the wall rises. As a result, the hydrodynamic boundary layer thickness and hence the skin friction decreases. $f'(0) \approx 1$, when there is no slip. Figs. 5-6 depict the effect of non-uniform heat generation/absorption parameters (A^*) and (B^*) on the temperature profiles of the flow. It is clear from the figures that an increase in the heat source/sink parameters enhances the temperature profiles of the flow. It is obvious to conclude that for lesser values of A^* and B^* there is all in temperature profiles, which reveals that negative values of A^* and B^* acts like heat absorption parameters and positive values as heat generators.

In the table 2, it is seen that the fluid parameter increases, the shear stress descends whereas the heat transfer rate increases. Shear stress decreases as an increase in the magnetic parameter. An enhancement of the heat source/sink parameter depreciates the heat transfer rate. Ascending slip parameter descends the skin friction coefficient, but increases the heat transfer rate.

Conclusions: The stagnation point flow of a MHD Powell-Eyring fluid over a nonlinearly stretching sheet in the presence of heat source/sink has been analysed. The following important observations can be derived from the numerical results:

The slip parameter influence depreciates the velocity. As the fluid parameter $K\Gamma (\ll 1)$ increases, the velocity profile increases whereas the temperature profile decreases. The skin friction coefficient also descends. The thermal boundary layer thickness increases for heat generation A^* and $B^* (< 0)$. The rate of heat transfer reduces as the temperature dependent heat generation enhances.

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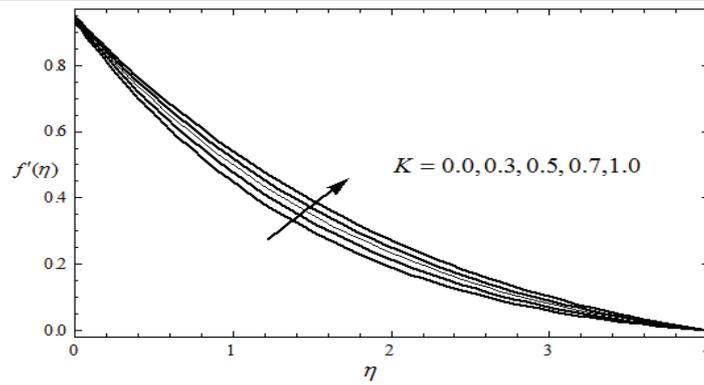


Fig.1 Velocity Profiles for different values of K

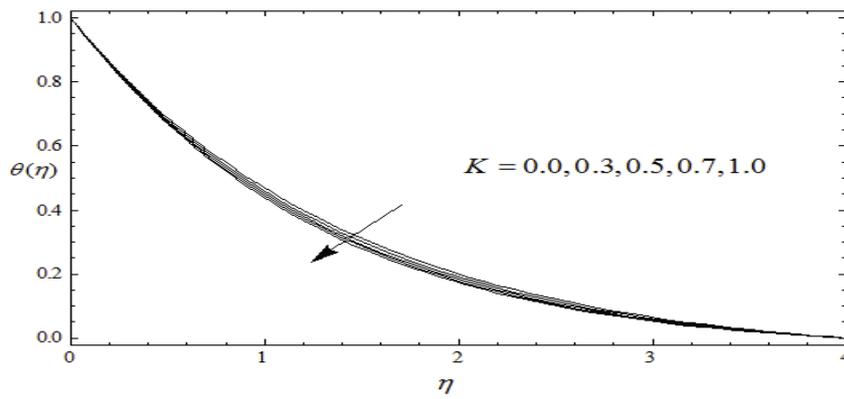


Fig.2 Temperature Profiles for different values of K

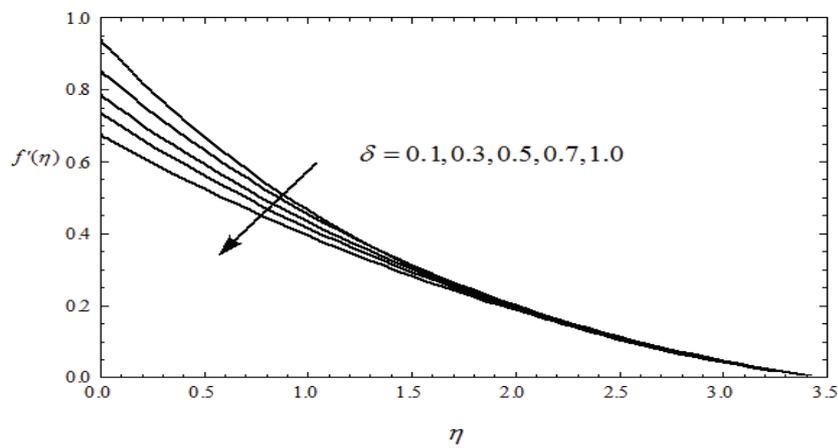


Fig.3 Velocity Profiles for different values of δ

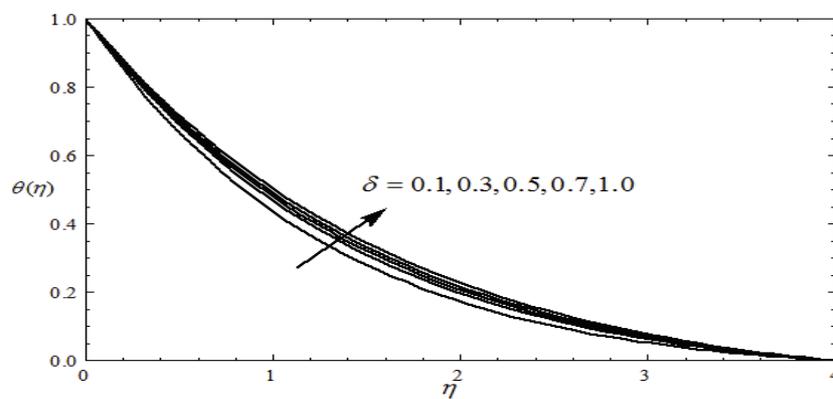


Fig.4 Temperature Profiles for different values of δ

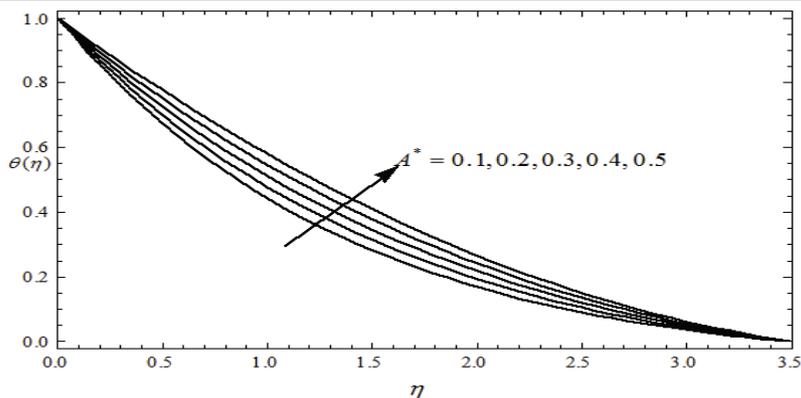


Fig.5 Temperature profiles for different values of A^*

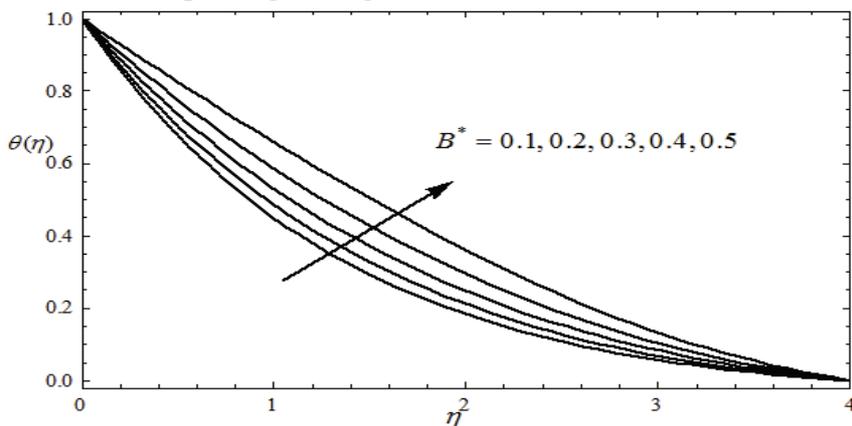


Fig.6 Temperature Profiles for different values of B^*

Table 1: Comparison of the rate of heat transfer when $K=\Gamma= A^*= B^* = \delta=0$.

Pr	Mahapatra and Gupta [15]	Raju et al. [16]	Present Results
0.05	-0.081	-0.0811	-0.08162
0.5	-0.383	-0.3833	-0.38342
1	-0.603	-0.6031	-0.60310
1.5	-0.777	-0.7772	-0.77682

Table 2 Computation of Wall Shear stress and Nusselt number for various pertinent parameters.

K	Γ	A^*	B^*	δ	$-f''(0)$	$-\theta(0)$	
0.1					0.841446	0.701558	
0.5					0.731961	0.730463	
1.0	0.1				0.646803	0.753311	
					0.83437	0.702948	
					0.825942	0.70463	
		0.1			0.841446	2.70143	
			0.3		0.841446	0.575588	
			0.5	0.1	0.841446	0.449617	
			0.3		0.841446	0.519352	
				0.5	0.1	0.841446	0.266889
					0.5	0.57684	0.620299
				1.0	0.422456	0.561383	

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